

ICORR 2023

ADDRESSING HYDROGEN PIPELINE REPURPOSING SAFELY & ECONOMICALLY

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Introduction

Challenges

Grades – an adequate metric for materials performance in H_2 ?

Repurposing strategies – if not Grades – then what?

Conclusions & roadmap

Introduction



We need H2

to meet
Paris Agreement

50-80%

consist of repurposed Existing natural gas grids



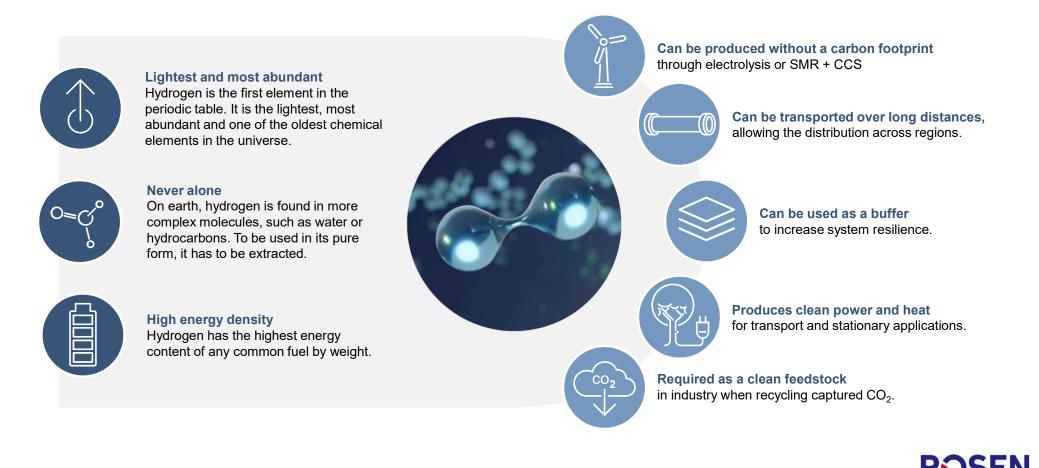


13% to 15%

of Energy Mix will be H2 and Ammonia

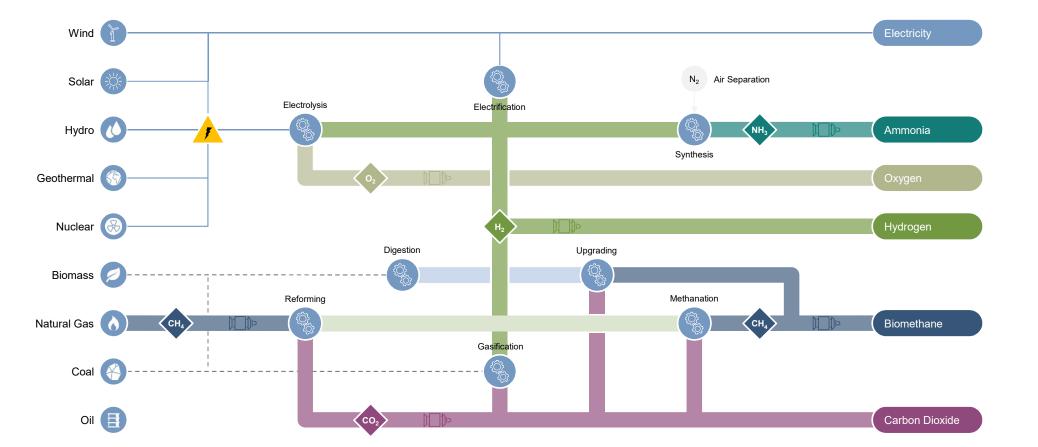
Heavy Industry & Long Transportation

The Role of hydrogen in the energy transition

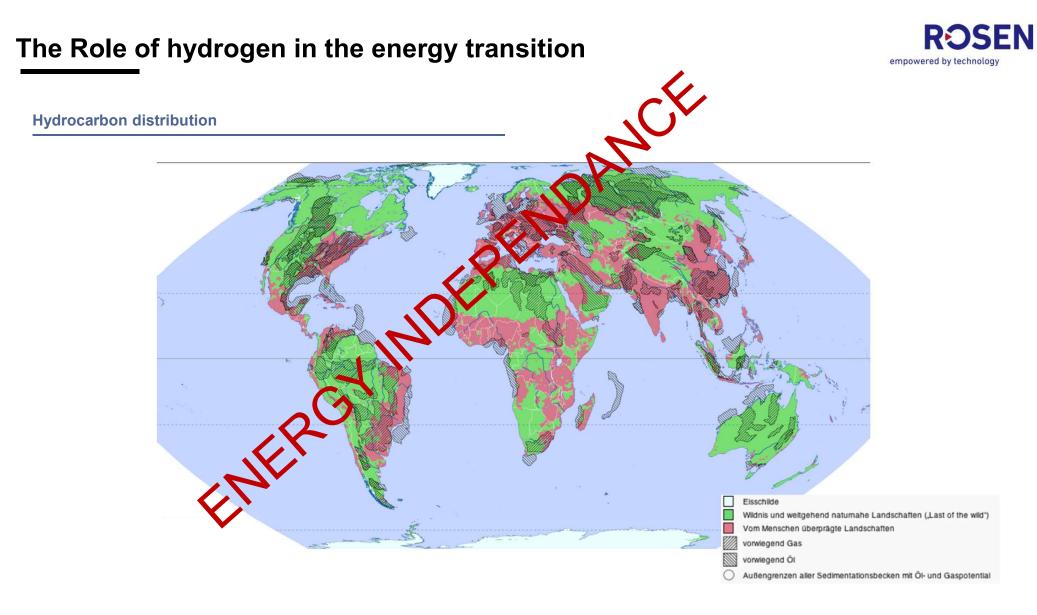


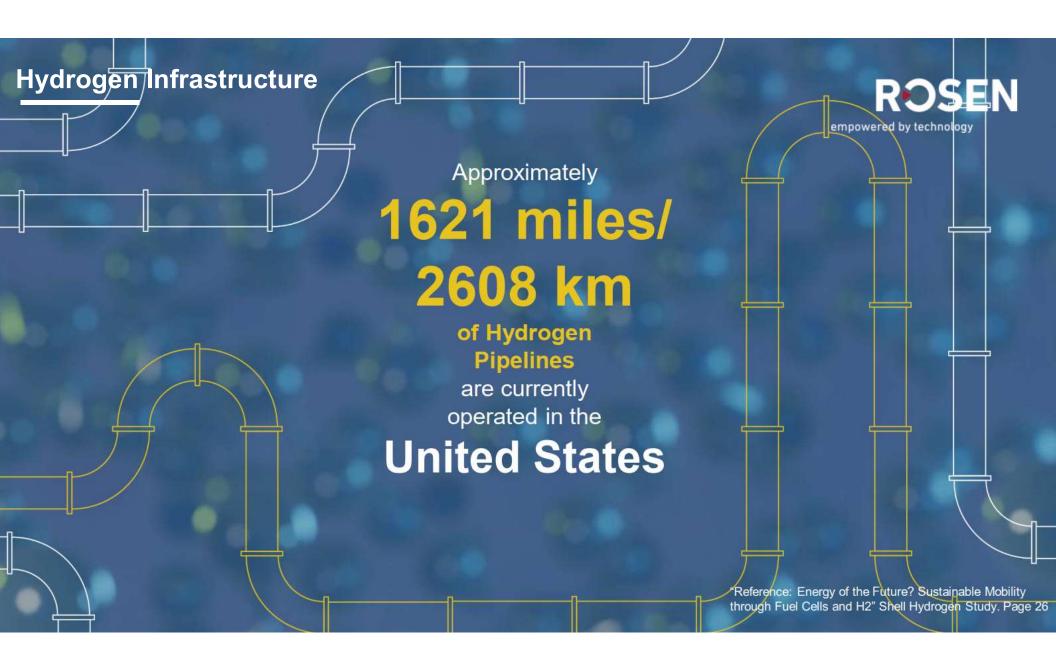
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The Role of hydrogen in the energy transition

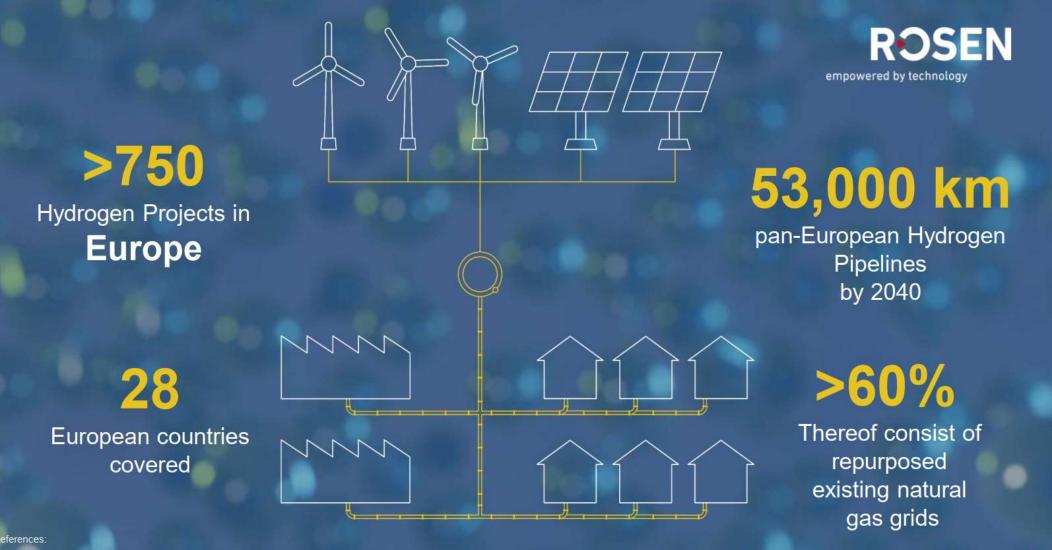








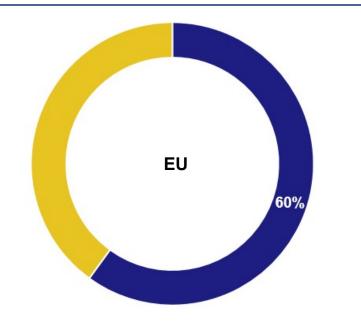




hb, European Hydrogen Backbone, A European Hydrogen Infrastructure Vision Covering 28 Countries, April 2022;

uropean Commission website, https://single-market-economy.ec.europa.eu/industry/strategy/industrial-alliances/european-clean-hydrogen-alliance_en

Role of pipeline Repurposing



H₂ Deployment at an industrial scale requires pipelines

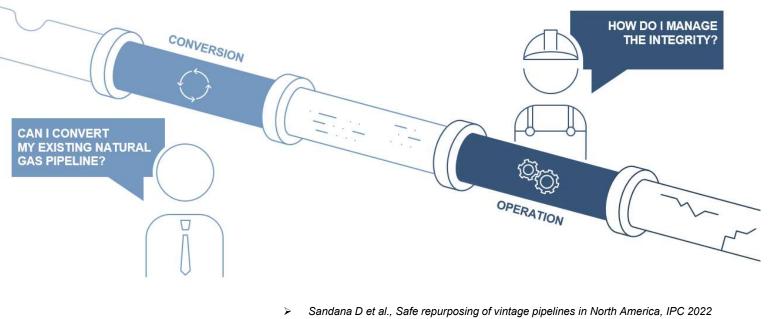
Repurposed NG pipelines ~10-35% of new construction costs

Repurposing in EU ... \in 0.2 million to \in 0.6 million / km

Cost / permit considerations \implies >50% of H₂ pipelines globally will be repurposed from NG pipelines



Managing repurposing safely



- > Safely Managing the Transition of Pipelines to H₂, E.-Peppler M et al. World H₂ congress 2021
- Existing pipeline materials and the transition to hydrogen, Gallon N et al., PTC 2021







REPURPOSING NATURAL GAS PIPELINES

Demonstrating the existing pipelines will remain fit-for-service under the new service

- The process requires the documentation of engineering inputs in order to inform the decision-making process for

 (i) the suitability to conversion, or if deemed necessary, for (ii) the development of practical economic rehabilitation and
 mitigation measures to achieve safe conversion.
- The key engineering inputs can be summarised as follows:
 - ✓ Identify Threats & Pipeline condition (baseline) e.g. vs. cracks.
 - ✓ Have an understanding of material 'DNA' & properties
 - ✓ Ensure Pipeline Risks remain ALARP under the new service
 - ✓ Identify necessary practical & economic intervention actions to address unreasonable risks
 - ✓ Define MAOP
 - ✓ Confirm adequacy of ratings of ancillary pressure-rated pipeline components e.g. valves, flanges



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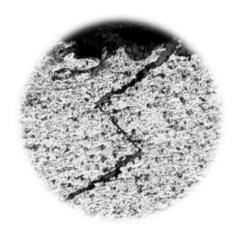
BUT... We need to tackle "new" mechanisms

\checkmark H₂ Embrittlement

Property	Effect of H ₂				
Strength	\leftrightarrow (?)				
Ductility	Ļ				
Fracture toughness	\downarrow				

✓ H_2 Fatigue (↑)

✓ H_2 – Environmentally – Assisted Cracking (HEAC)

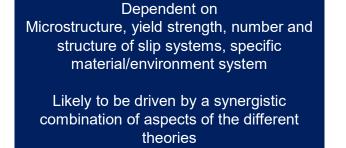


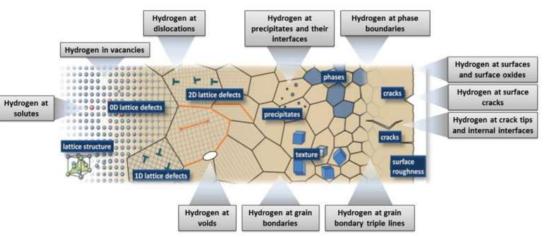


Impact of hydrogen vs materials

HE Mechanisms usually quoted

- Stress Induced Hydride formation and cleavage Metals with stable hydrides (Group Vb metals, Ti, Mg, Zr and alloys)
- Hydrogen-Induced Decohesion (HEDE)
- Hydrogen-Enhanced localised Plasticity (HELP)
- Adsorption-Induced Dislocation Emission (AIDE)

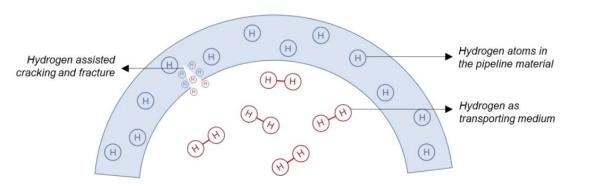








Impact of hydrogen vs materials

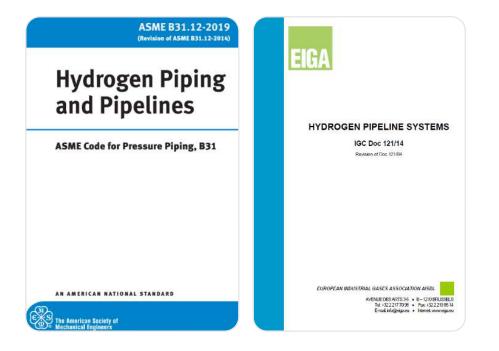


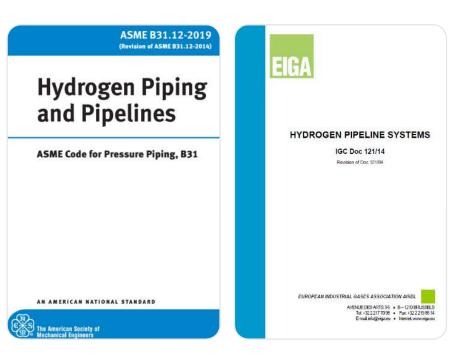
HEAC

Cracking believed to solely take place in the presence of pre-existing flaws or cracks (outside fatigue)

Cracking in bulk material away from cracks? (stress raisers, hard spots, etc.)







 EIGA / AIGA / CGA Guidelines:

 "it is recommended that only lower strength API 5L grades

 (X52 or lower) be used"

<u>ASME B31.12 Option A</u>: Materials Performance Factor penalises >X52

IGEM TD/1 Supplement 2:

Penalises >X52

EIGA / AIGA / CGA Guidelines:

"This good service [of $\leq X52$] is attributed to the relatively low strength of these alloys, which imparts resistance to hydrogen embrittlement and the other brittle fracture mechanisms"



Preference for lower grades

Option A (prescriptive / No H₂ testing)

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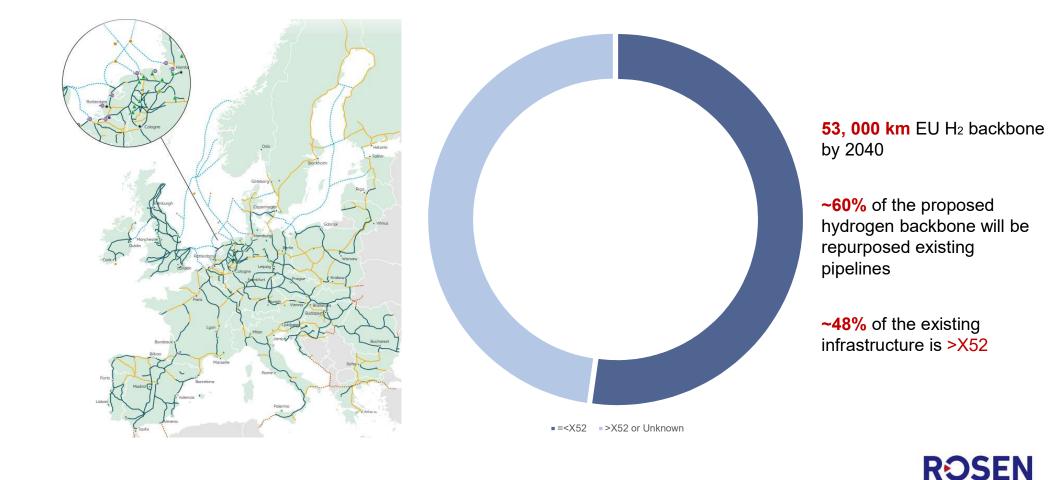
Design Pressure (NG) $P = \frac{2.S.t}{D}$. F. E. T Vs. (H₂) $P = \frac{2.S.t}{D}$. F. E. T. H_f Materials performance factor in H₂ Table IX-5A Carbon Steel Pipeline Materials Performance Factor, H_f Specified Min. Strength, ksi System Design Pressure, psig 2,600 Tensile Yield ≤1,000 2,000 2,200 2,400 **Design Factor** 66 and under ≤52 1.0 1.0 0.954 0.910 0.880 Over 66 through 75 ≤60 0.874 0.874 0.834 0.796 0.770 Over 75 through 82 ≤70 0.776 0.776 0.742 0.706 0.684 Class Over 82 through 90 ≤80 0.694 0.694 0.662 0.632 0.610 NG H_2 location 0.72 1 0.5 2 0.60 0.5 0.50 0.5 3 4 0.40 0.4

Preference for lower grades

Design Pressure NG vs H ₂ 32 " diameter, 13.4 mm wall thickness, grade X70 / L485 pipele							
ASME Location Class	P _{H2} / bar per ASME B31.12 – Option A	P _{H2} / bar per IGEM/TD/1 Supplement 2*	P _{NG} / bar per ASME B31.8	Reduction in Pressure for H2 (B31.12 / TD/1) Compared to NG / %			
1 Div 2	61	59	114	47 / 48			
2	61	59	95	36 / 38			
3	61	59	79	23 / 25			
4	49	47	63	23 / 25			



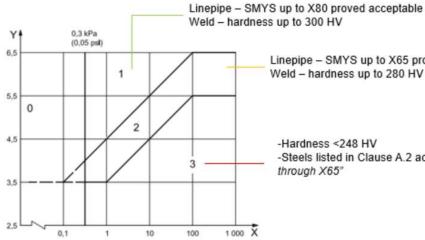
Prescriptive codes vs. Hydrogen Chain Value Challenges



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Use of high grades in hydrogen charging services?



Linepipe - SMYS up to X65 proved acceptable

-Hardness <248 HV -Steels listed in Clause A.2 acceptable e.g. "A and B and X42

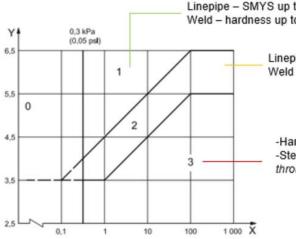
Sour service Application

ISO 15156 / MR 0175

- HE generally controlled by hardness restrictions ٠ (<248 HV) for most severe applications
- But grades up to X65 approved by standard ٠
- Use of high strength grades up to X80 also acceptable in milder H₂S



Use of high grades in hydrogen charging services?



Linepipe – SMYS up to X80 proved acceptable Weld – hardness up to 300 HV

> Linepipe – SMYS up to X65 proved acceptable Weld – hardness up to 280 HV

-Hardness <248 HV -Steels listed in Clause A.2 acceptable e.g. "A and B and X42 through X65"

Sour service Application

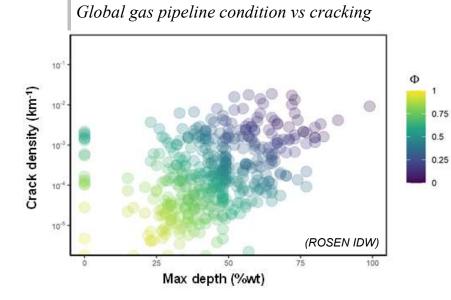
Caution

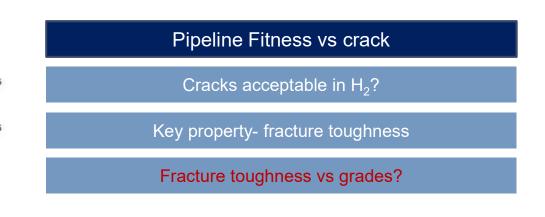
Pipeline grades not equal (vs. age)

Validity of the sour standard requirements shall be cautioned against its year of revision and the quality of manufacturing and construction applicable at the time

Example illustrates the conservatism that may exist around unduly punishing the use of grades above X52

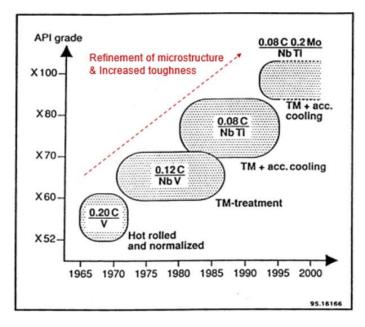
Pipeline FFS in H_2 – Other key materials properties & correlation with grades?







Pipeline FFS in H_2 – Other key materials properties & correlation with grades?



Fracture toughness vs grades?

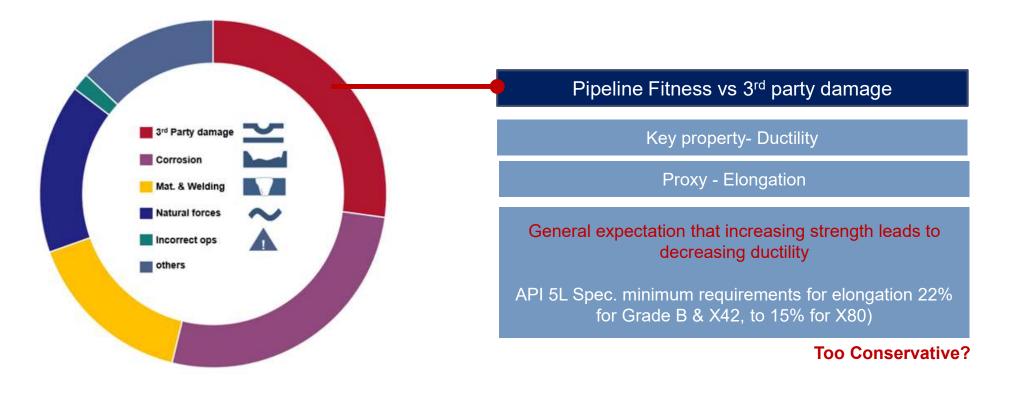
Properties as tested for a low strength (<X52) and a high Strength (X70) steel

Grade	YS (ksi)	UTS (ksi)	Y/T	Uniform Elongation (%)	Location	Test Temperature	Individual Impact Energy (J)	Shear Area (%)
X42 / L290	53	72	0.74	35	Pipe body	0°C	19, 16, 18	80, 70, 70
X70 / L485	72	96	0.75	34	Pipe body	0°C	308, 258, 275	100, 100, 100

► If anything, higher grade = higher specified toughness

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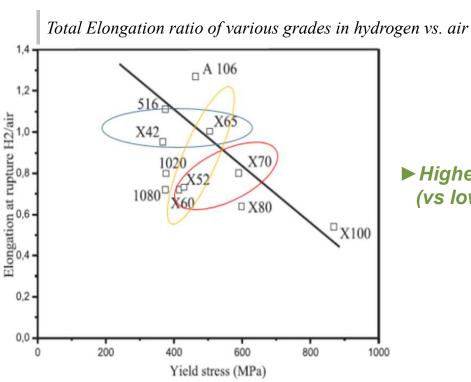
Pipeline FFS in H_2 – Other key materials properties & correlation with grades?

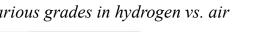




Pipeline FFS in H₂ – Other key materials properties & correlation with grades?

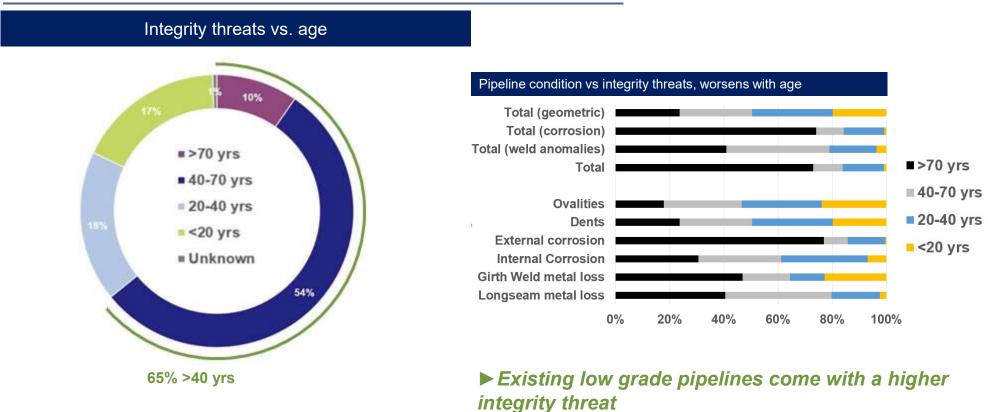
Elongation vs grades?





► Higher grades ≠ bad suitability in all cases (vs low grades)



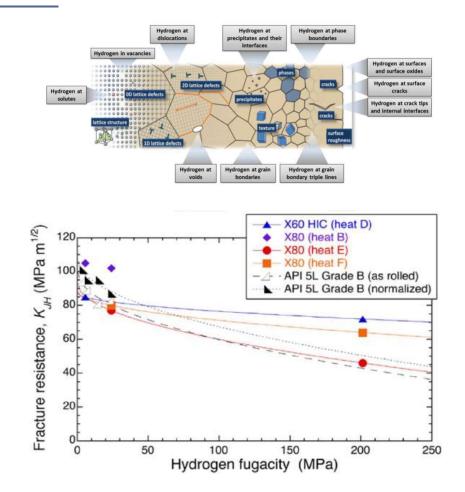


Pipeline FFS in H_2 – Other key materials properties & correlation with grades?

Sandana D et al., Safe repurposing of vintage pipelines in North America, IPC 2022

Importance of microstructure

- **HE is a multivariate and complex problem**, from which variables associated with the microstructural (e.g. phases, chemistry) and macroscopic (e.g. grade, mechanical properties, stresses) level cannot be independently extracted and assessed in isolation.
- Line pipe materials of a same nominal grade are not all equal against HE susceptibility and hydrogen service
 - Overlaps between different domain of microstructures and pipe grades.
 - A grade can be achieved by different process routes and therefore microstructures.



Predicting performance = f (grade, microstructure, chemistry)?

- 2 steels with very similar chemistry
- And Identical Nominal Grade (X52M)

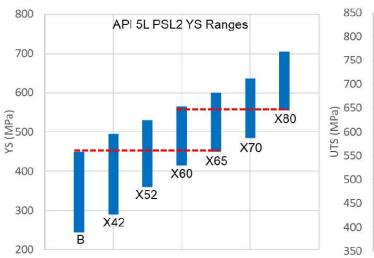
Material	Element Concentration (wt.%)									
Material	С	Mn	Si	Р	S	AI	Nb	V	Ti	
MTR 1	0.04	1.06	0.20	0.01	0.001	0.03	0.03	-	0.01	
MTR 2	0.04	1.07	0.21	0.01	0.002	0.034	0.032	-	0.014	

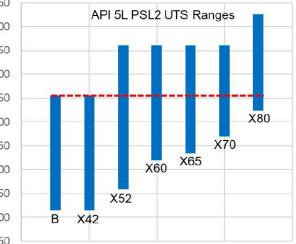
But very different mechanical properties

Material	Grade	YS (ksi)	UTS (ksi)	Ү/Т
MTR 1	X52M	78.7	81.2	0.97
MTR 2	X52M	61.1	72.4	0.84

"Nominal" pipe grade vs. actual strength

- Pipe grade as a proxy to strength in order to discriminate the performance of line pipe materials in H₂
- Current guidelines favor the use of low strength grades up to X52
- But grade is not even a good predictor of actual pipe strength







- 1. Predicting performance = f (grade, microstructure, chemistry)? Challenging
- 2. Assume specified minima Charpy energies, convert to "true" fracture toughness and apply a "knockdown" factor to account for hydrogen
 - Charpy data may not exist for many pipelines (pre-2000 and PSL 1)
- 3. Assume hydrogen is the "great leveller" and that hydrogen affected fracture toughness for all steels converges around the same level (~50 ksi.in^{1/2} / 55 MPa.m^{1/2})
 - Limited empirical data supporting this, no compelling mechanistic justification available, may be over- or nonconservative



Materials 'performance' behaviour under H₂?

- Guidelines ... undue conservatism?
- Is a steel <= X52 automatically suitable? (hard spots, heavy banding, etc.)
- Is a steel > X52 inevitably unsuitable? (X65 / X70... Sour service)

Severity of hydrogen issues (e.g. reduction in toughness, crack susceptibility) largely modulated by steel microstructures and chemistries rather than just grade

Testing of representative linepipe materials

ASME B31.12 - Option B



Materials 'performance' behaviour under H₂?

Emphasis

understanding of the actual pipeline material (s) population and DNA, and the testing of representative linepipe materials 'performance' behaviour under $\rm H_2$

□ ASME B32.12, PL-3.21

Conduct material sampling every 1 mile (1.6 km)

- Where do we need to SAMPLE? (TVC materials certificates – incomplete or missing)
- Cost effectiveness? Practicality?





Materials 'performance' behaviour under H₂?

Emphasis

understanding of the actual pipeline material (s) population and DNA, and the testing of representative linepipe materials 'performance' behaviour under $\rm H_2$

□ ASME B32.12, PL-3.21

Conduct material sampling every 1 mile (1.6 km)

ROSEN Approach

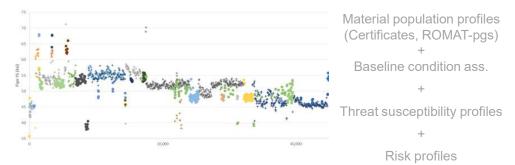
Material population & Risk- driven approach

► Where do we need to SAMPLE?

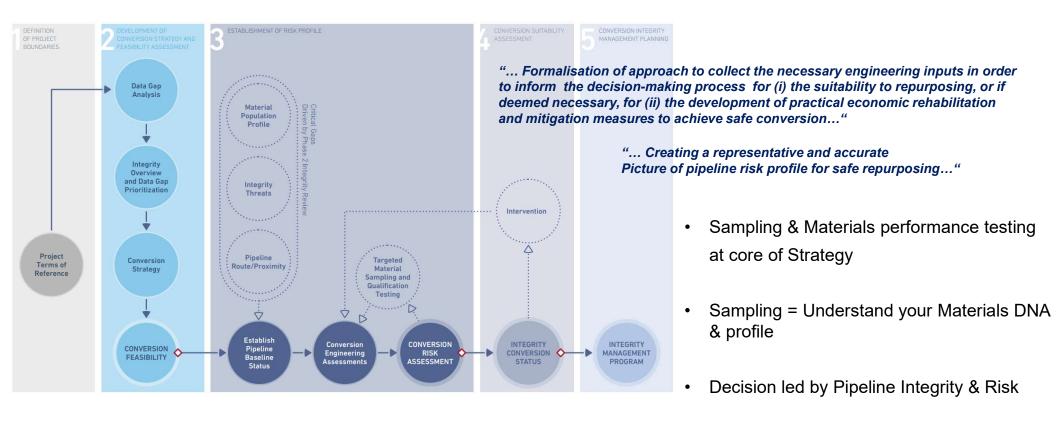
(TVC materials certificates – incomplete or missing)

Cost effectiveness? Practicality?

development of TARGETED linepipe sampling strategies by integrating the knowledge of materials populations, threat susceptibility profiles, baseline condition and consequences.



Conclusions – ROSEN Hydrogen Integrity Roadmap



- Sandana D et al., Safe repurposing of vintage pipelines in North America, IPC 2022
- > Ruiz Martinez et al. A practical guide to repurpose existing pipelines for transporting H2, OMC 2023

