



Advisory – Corrosion in Pipelines

Corrosion Awareness Day, 2026

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LR Offshore Technical Support Offshore

Aims of presentation

- Introduction to Advisory
- Introduction to corrosion in pipelines
 - Corrosion mechanisms
- Corrosion defect assessment case study
 - Review of data
 - Assessment methodology
 - Results



Introduction to Advisory

A Trusted Advisor, partnering with clients to tackle business challenges



ASSET PERFORMANCE

Define actionable recommendations to optimise asset performance



MANAGEMENT CONSULTING

Prepare your business for future challenges



INNOVATION

De-risk and implement new technologies to future-proof your assets



OPERATIONAL SERVICES

Protect your assets throughout their lifecycle to deliver your contractual obligations and minimise risk



ENERGY TRANSITION

Build and execute robust strategies to navigate the Energy Transition



ASSET & RISK MANAGEMENT

Creating a safer and more efficient operating environment



PROJECTS ADVISORY

Optimise the value of your project investments



HUMAN ELEMENT

Apply Human Factors specialist expertise to enhance operational performance



Introduction to Advisory

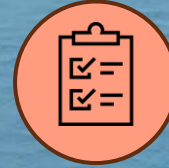
Asset performance



Aging Assets and Rising Maintenance Costs



Decarbonisation Imperative



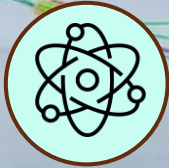
Emissions Reporting Complexity



Regulatory Complexity



Noise and Vibration Risks



Uncertainty in Technology Performance



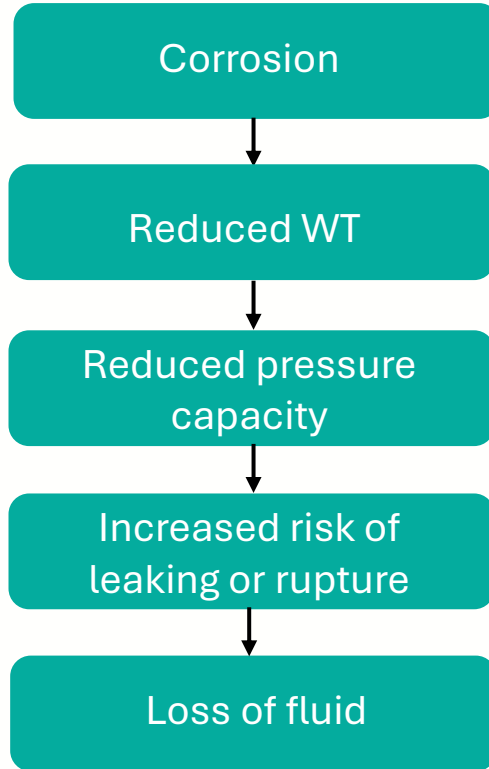
Lifetime Extension



LR Advisory's structure comprises multidisciplinary experts who understand the intricacies of maritime and energy operations to provide client with evidence-based strategic advice on critical issues such as digitisation, energy transition, safety and commercial success

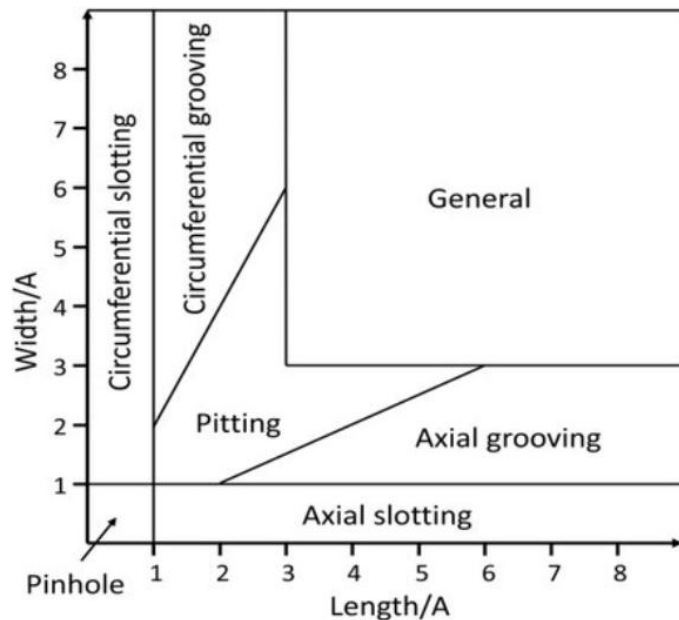
Corrosion in pipelines

Issues



Corrosion in pipelines

Types of metal loss features

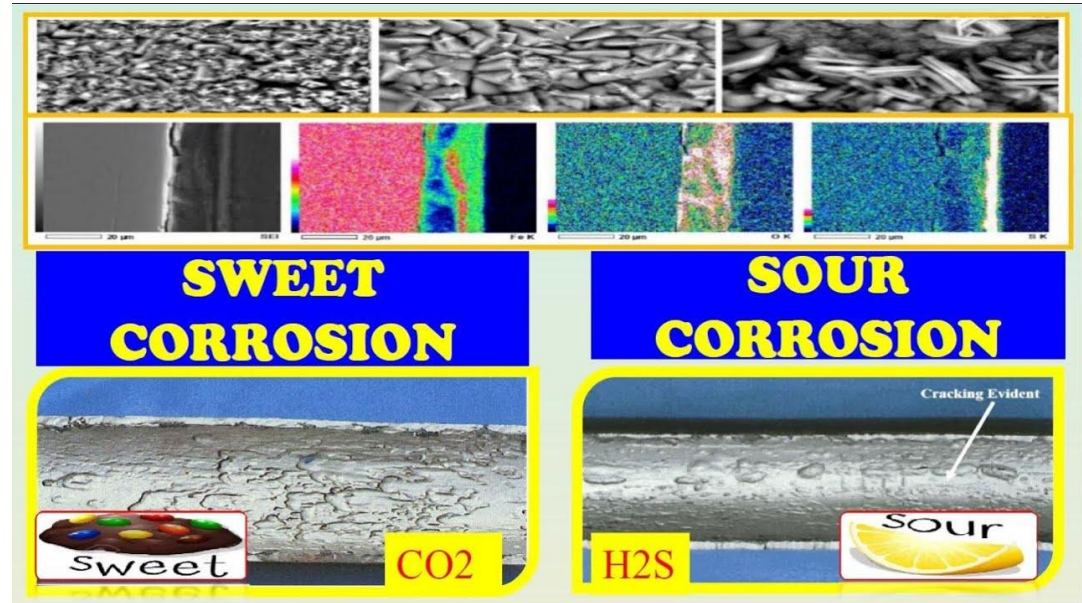


Anomaly dimension class	Definition	Reference point/size for the POD in terms of $l \times w$
General:	$\{[w \geq 3A] \text{ and } [l \geq 3A]\}$	$4A \times 4A$
Pitting:	$\{([1A \leq w < 6A] \text{ and } [1A \leq l < 6A] \text{ and } [0.5 < l/w < 2]) \text{ and not } ([w \geq 3A] \text{ and } [l \geq 3A])\}$	$2A \times 2A$
Axial grooving:	$\{[1A \leq w < 3A] \text{ and } [l/w \geq 2]\}$	$4A \times 2A$
Circumferential grooving:	$\{[l/w \leq 0.5] \text{ and } [1A \leq l < 3A]\}$	$2A \times 4A$
Pinhole:	$\{[0 \text{ mm} < w < 1A] \text{ and } [0 \text{ mm} < l < 1A]\}$	Minimum dimensions to be further defined by Contractor, see table A3-2
Axial slotting*:	$\{[0 \text{ mm} < w < 1A] \text{ and } [l \geq 1A]\}$	$2A \times \frac{1}{2}A$
Circumferential slotting*:	$\{[w \geq 1A] \text{ and } [0 \text{ mm} < l < 1A]\}$	$\frac{1}{2}A \times 2A$

Corrosion in pipelines

Internal corrosion mechanisms

- Key issue = what's in the pipe
- Sweet corrosion
 - Most common internal corrosion mechanism
 - CO₂ dissolved in water
 - Siderite films are formed
 - Below 60°C – General corrosion
 - Above 60°C – Pitting corrosion
- Sour corrosion
 - Less common than sweet corrosion
 - H₂S dissolved in water
 - Can result in pitting and cracking



Corrosion in pipelines

Internal corrosion mechanisms



- MIC
 - Caused by bacteria on pipe wall
 - These consume sulphates and produce H_2S
 - Can be introduced via untreated seawater
 - Can form a groove along the 6 o'clock position



Corrosion in pipelines

External corrosion mechanisms

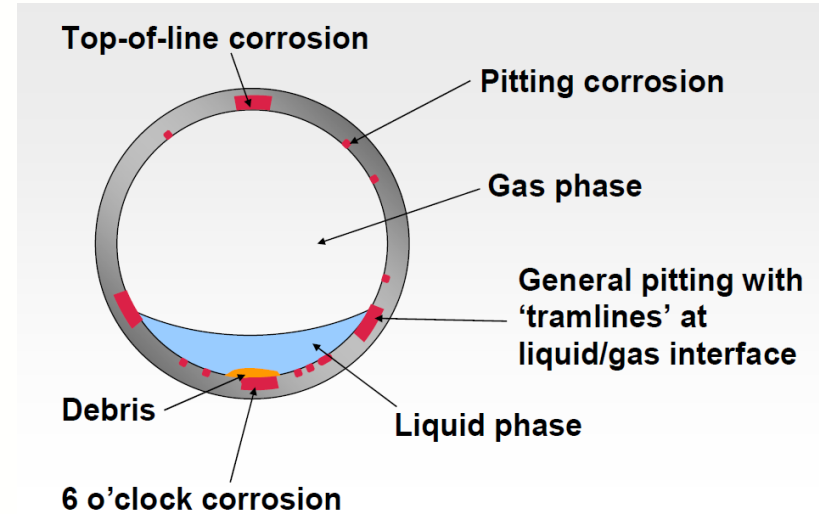
- Oxygen corrosion
 - Subsea pipelines – exposed to seawater and dissolved O_2
 - Onshore pipelines – exposed to moisture and O_2
 - Corrosion occurs if barriers are broken

Corrosion in pipelines

Internal corrosion locations

Some areas are particularly vulnerable to corrosion:

- Top of pipe
 - Issue in high temperature wet gas and multiphase lines
- Bottom of pipe
 - Due to water settling out
 - MIC can result in a groove at 6 o'clock position
- Bends
 - Combined erosion & corrosion



Corrosion in pipelines

External corrosion locations

Some areas are particularly vulnerable to corrosion:

- Riser splash zone
 - Steel is exposed to seawater and atmospheric corrosion
 - Repeated wetting and drying
 - Ineffective cathodic protection

Case Study

Corrosion Defect Assessment of Thistle Alpha Export Line

Background:

- Thistle to Dunlin 16" crude oil pipeline
- Started exporting in 1978
- Length: 12.2 km
- ILI and FFP completed in 2001 & 2009



Case Study

Corrosion Defect Assessment of Thistle Alpha Export Line

Objectives:

- Operator requested LR review ILI results
- Determine if the pipeline was fit for purpose
- Determine the pipeline remnant life

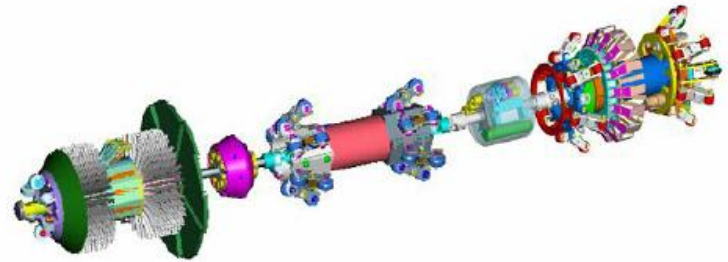


Case Study

The inspection – findings

Data:

- 460 external corrosion features
- 63399 internal corrosion features



Case Study

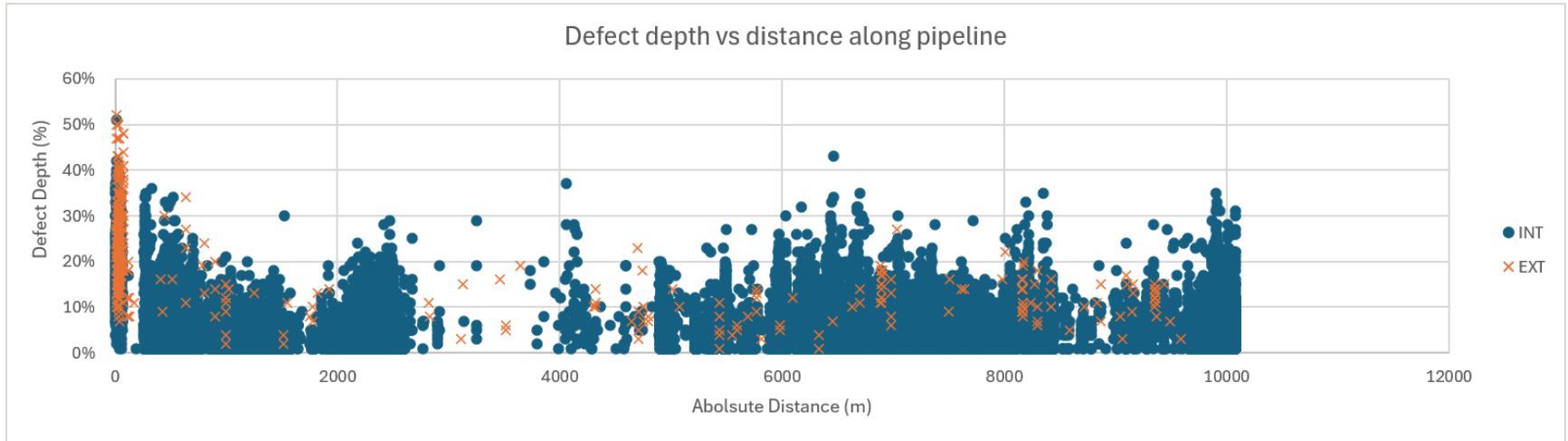
The inspection – inspection issues

Issues:

- Significant wax deposition
- The ILI tool was out with the optimal velocity range between KP 8.4 and KP 12.5
- Power loss occurred at KP10.2

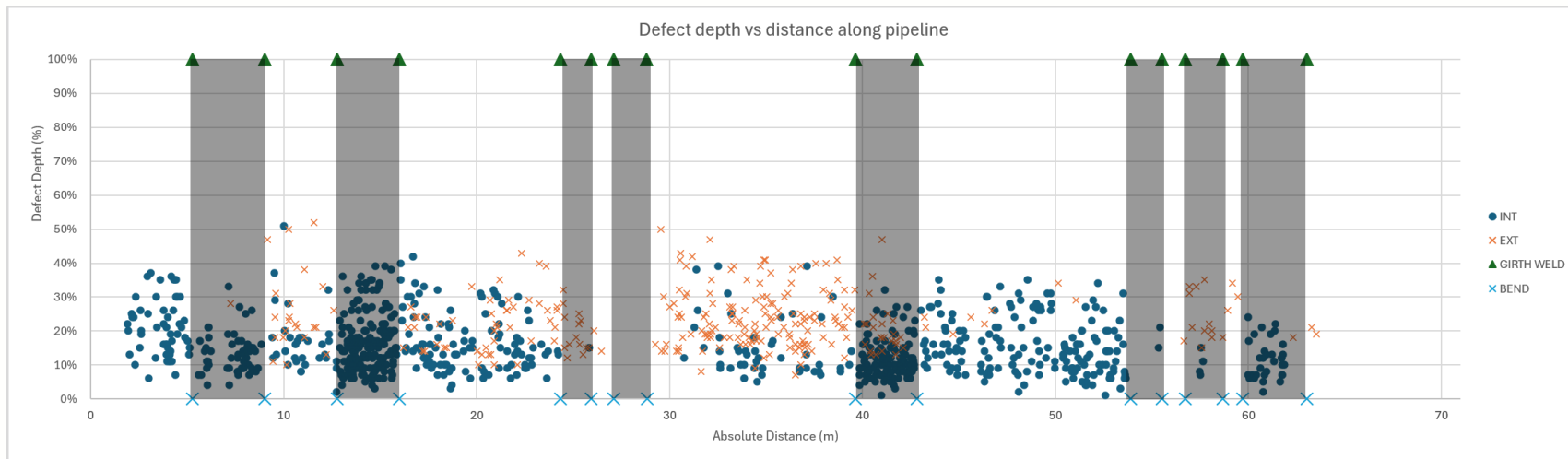
Case Study

The inspection – data deep dive



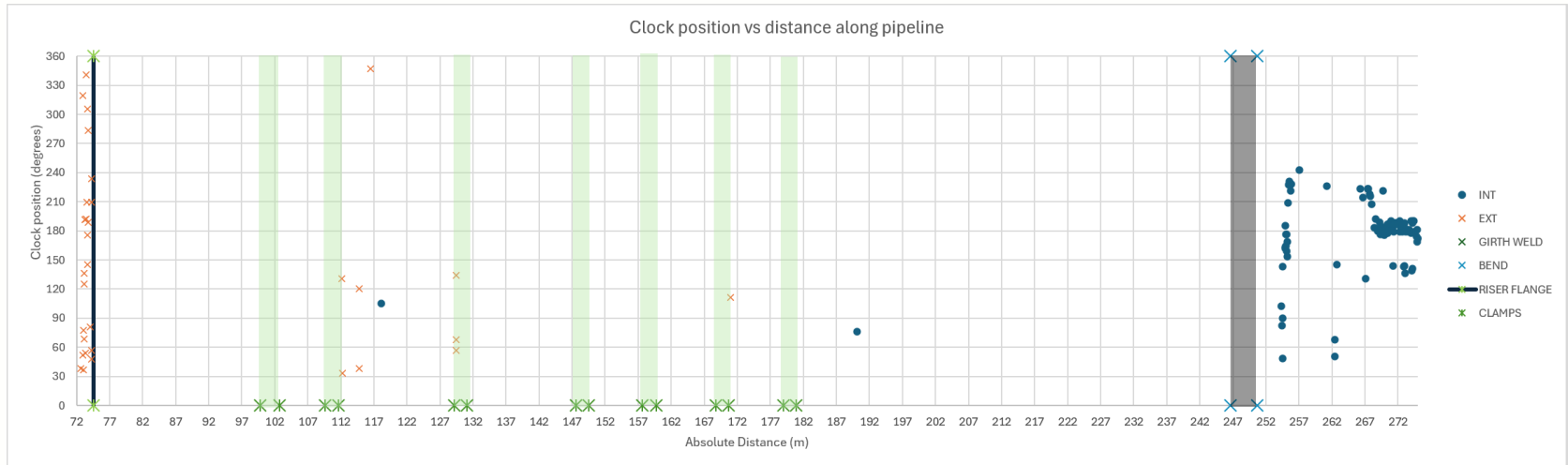
Case Study

The inspection – data deep dive



Case Study

The inspection – data deep dive

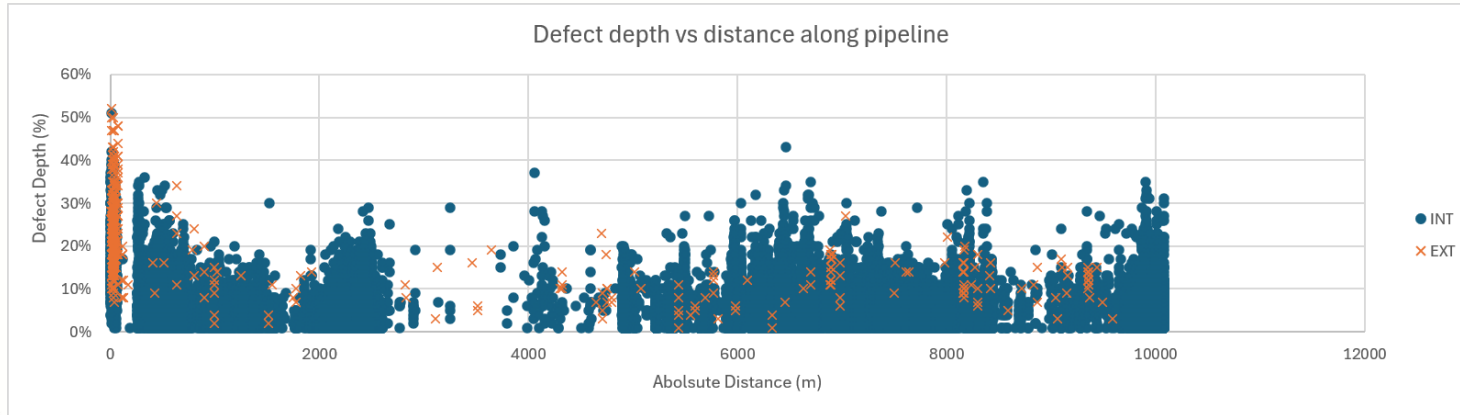


Case Study

The inspection – data deep dive

Points of interest:

- Majority of external defects located within riser/topsides
- External defects located within subsea pipeline. Note the pipeline has a:
 - 9.5 mm thick corrosion coating
 - 36.6 mm CWC



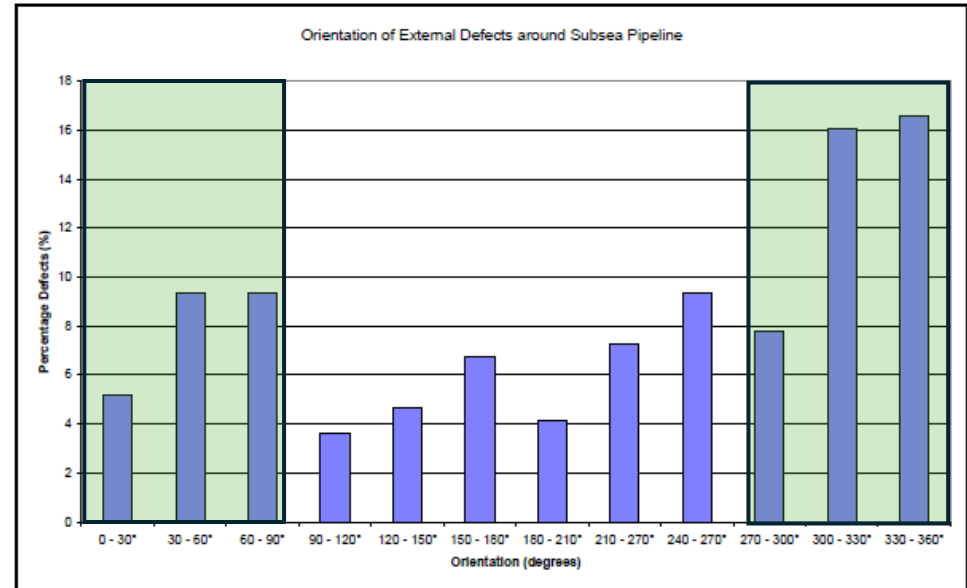
Case Study

The inspection – data deep dive



Reasons for external corrosion in subsea pipeline:

- Likely pipeline is not fully buried
- Likely CWC and corrosion coating damage
 - Majority of features located within top half of pipe



Case Study

The inspection – data deep dive - conclusions

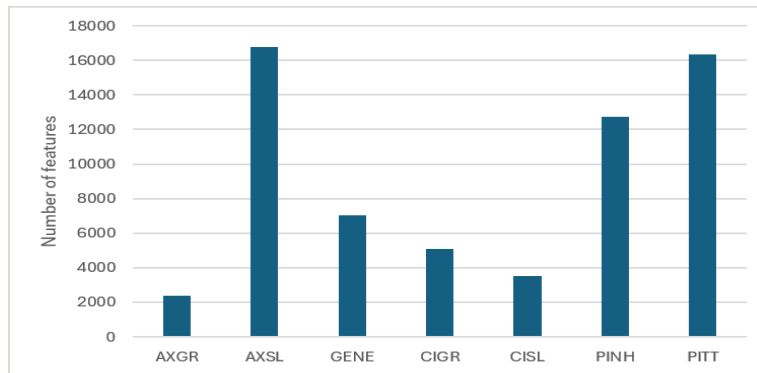
From the data review alone, LR was able to inform of operator:

- Possible presence of MIC
 - Untreated seawater in the line
 - Possible biocide injection required
- External coating damage
 - Topsides/ Riser
 - Subsea pipeline

Case Study

Methodology

- Data also noted both axial and circumferential features
- The defects were assessed using 2 different methods:
 - DNV-RP-F101 method
 - Kastner method

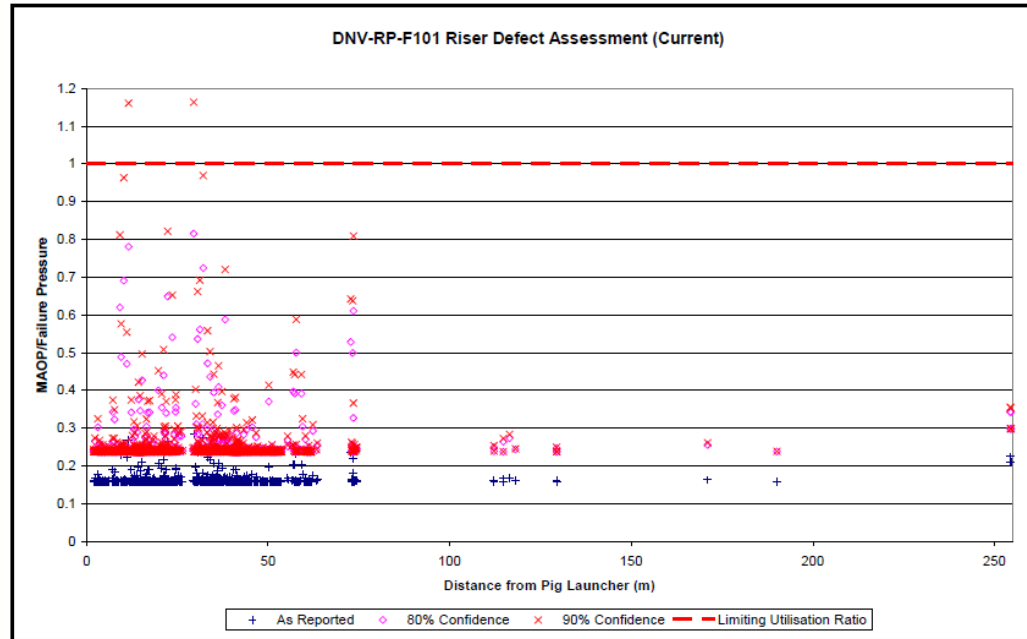


DNV	Kastner
Axial defects	Circumferential defects
Bursting	Plastic collapse
Pipeline pressure / Failure pressure	Axial tensile stress / Axial failure stress

By using both methodologies, a complete picture of pipeline condition could be determined

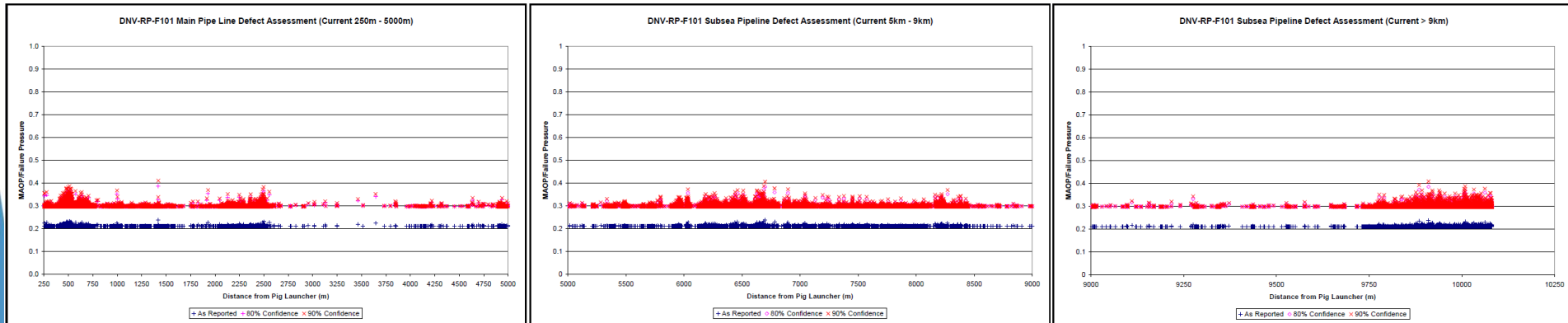
Case Study

Results: DNV-RP-F101 topside and riser assessment
(current)



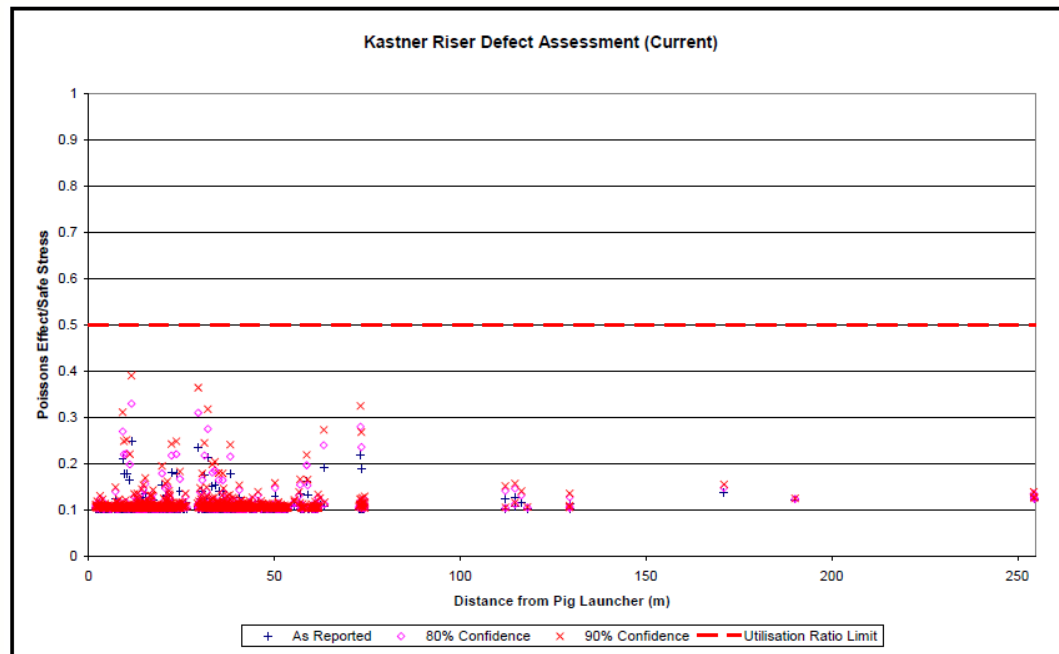
Case Study

Results: DNV-RP-F101 subsea pipeline assessment (current)



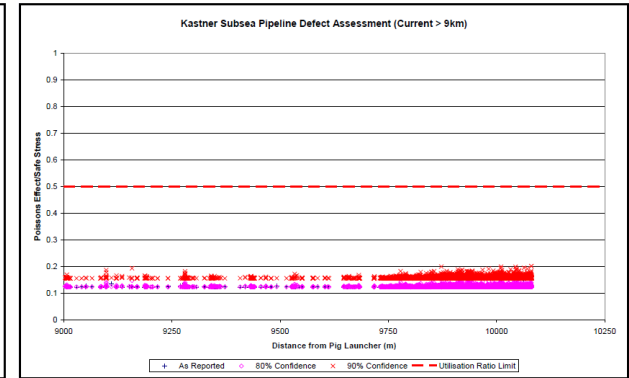
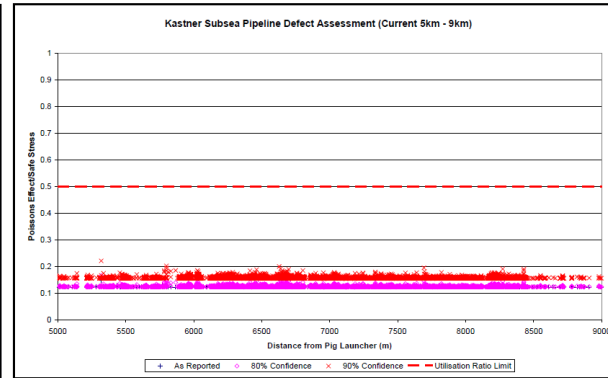
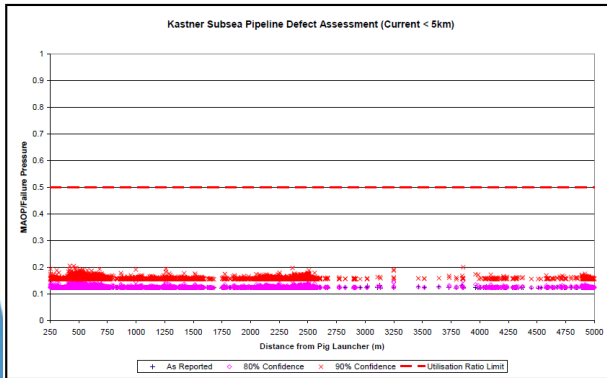
Case Study

Results: Kastner topside and riser assessment
(current)



Case Study

Results: Kastner subsea pipeline assessment (current)



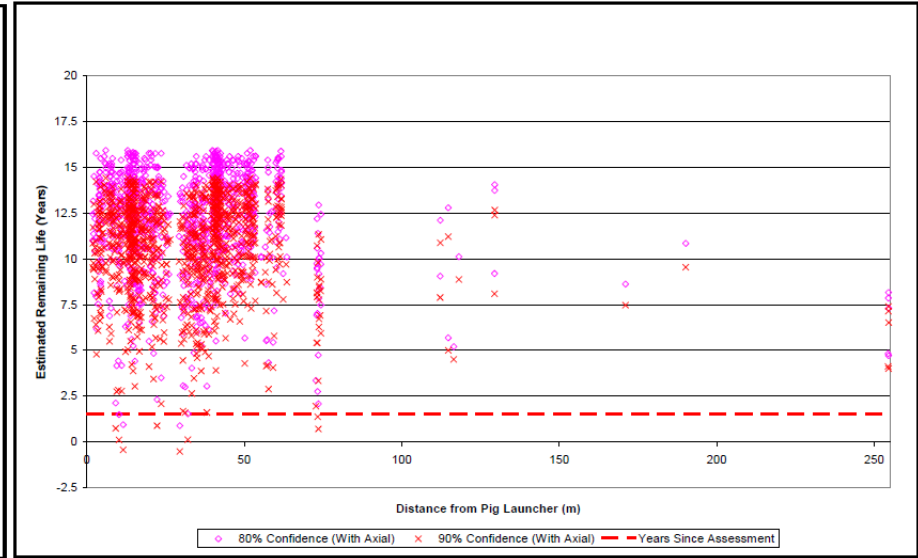
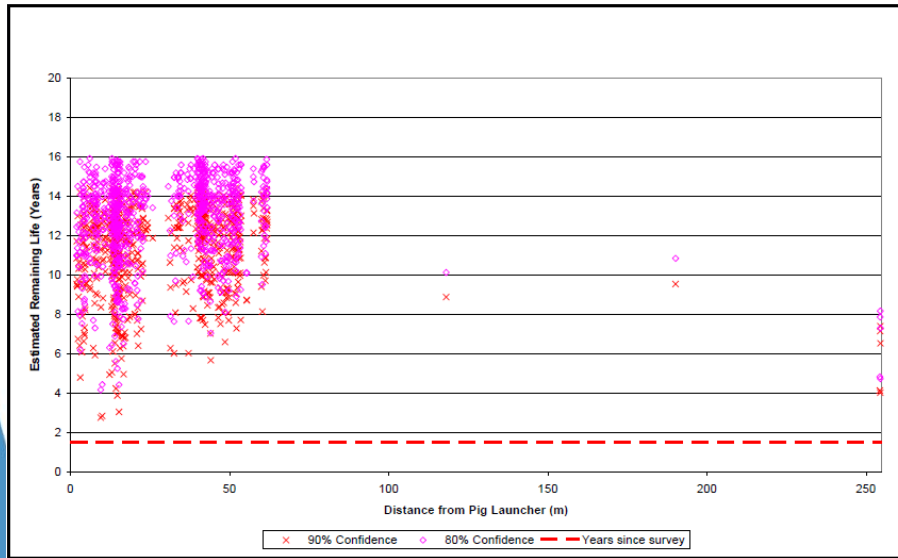
Case Study

Corrosion rates

- Once LR had reviewed current condition, the remnant life was determined.
- Features are “grown” until code violation
- Corrosion rate: 0.65 mm/year
- Based on max observed rate between 2001 and 2009

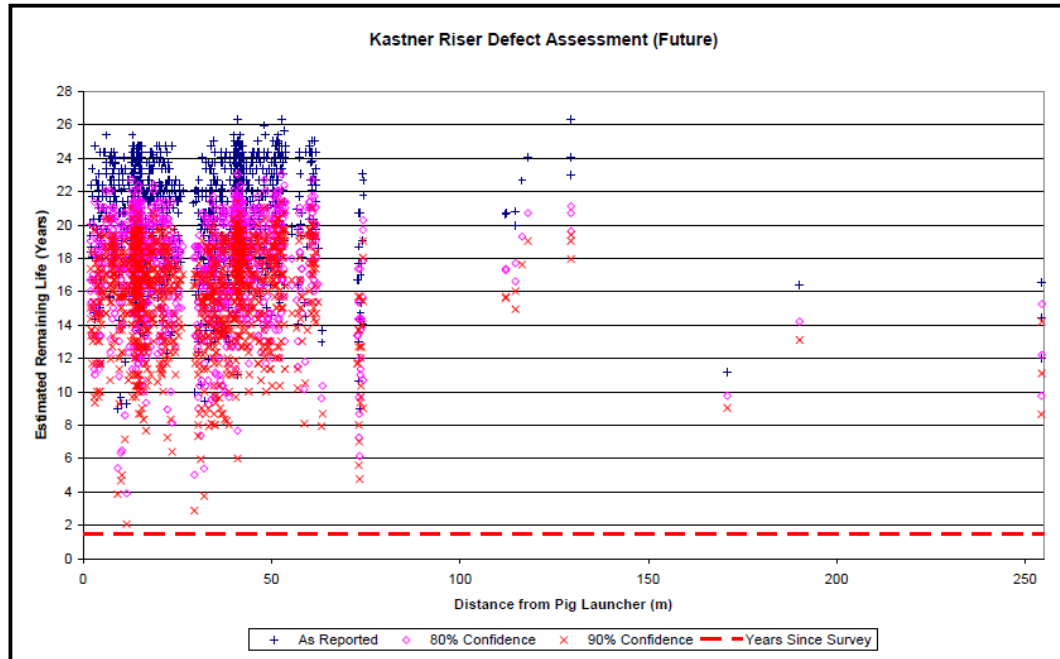
Case Study

Results: DNV-RP-F101 topside and riser assessment
(future)



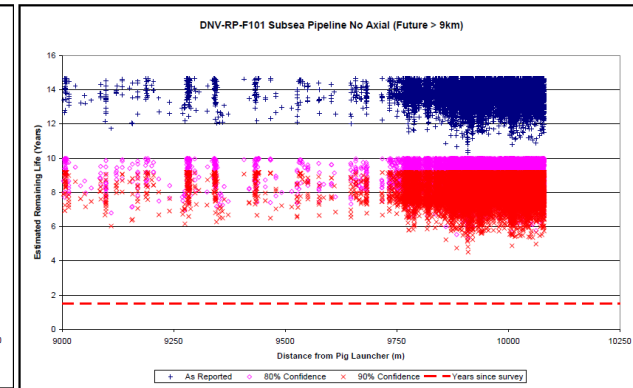
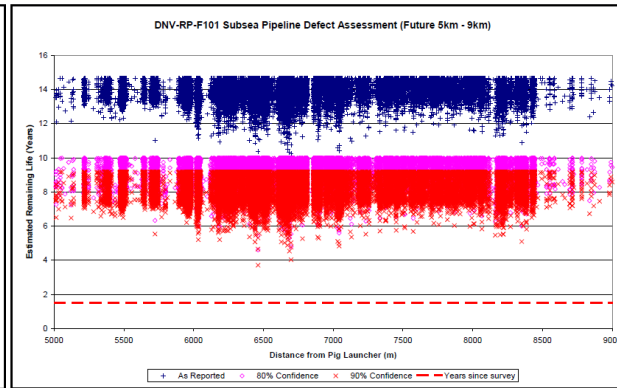
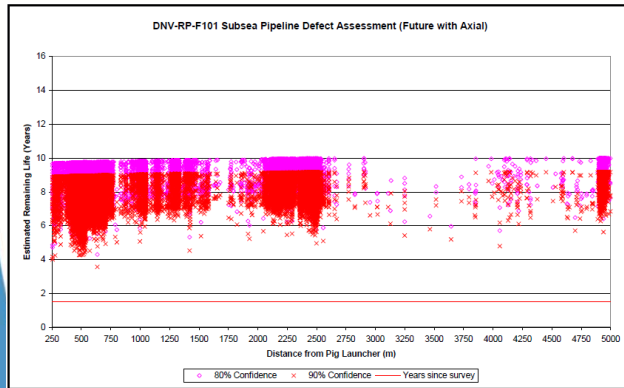
Case Study

Results: Kastner topside and riser assessment
(future)



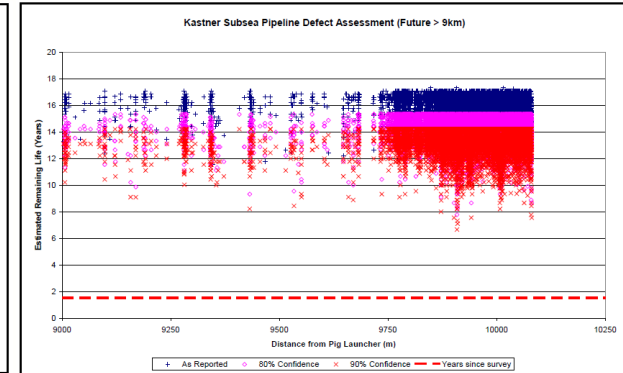
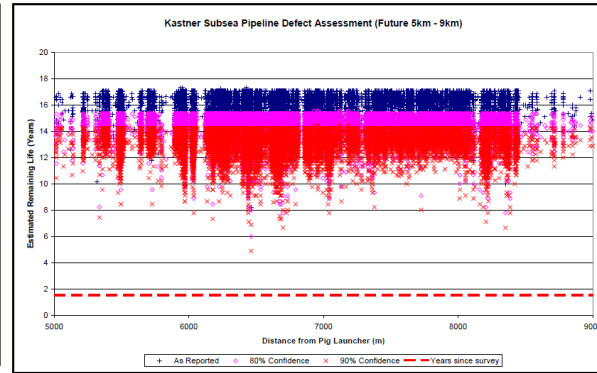
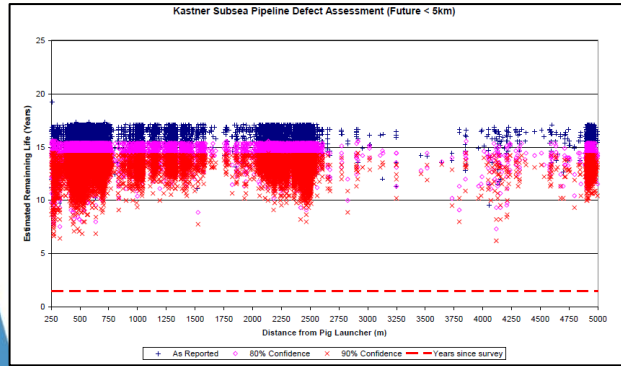
Case Study

Results: DNV-RP-F101 subsea pipeline assessment (future)



Case Study

Results: Kastner subsea pipeline assessment (future)



Case Study

Key conclusions from assessment

- Governing external feature was located topsides
 - Defect dimensions at the time of measurement were beyond the allowable code limits
 - LR recommended an immediate repair of all external features
 - This was completed in 2010
- Governing internal feature was located topsides
 - Remnant life of 1.3 years
 - LR recommended that the 10 worst case topside features be inspected further
- LR recommend that ILI is reperformed as soon as possible
 - Missing 1.9 km
 - Possible inaccuracies

Case Study

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Thank you for your attention

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